

INVESTIGATION ON SURFACE INTEGRITY OF SS316L 3D PRINTED STENT**Mr. Rohit P. Jadhav**

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Abstract:

This investigation focuses on the analysis of the surface integrity of a Stainless Steel 316L (SS316L) powder stent manufactured using Selective Laser Melting (SLM) technology. In the present work different post-processing methods viz. stress-relieved, electropolished, stress-relieved and electropolished, and without stress-relieved and without electropolished were studied in correlation with the SLM process in the context of stent surface characterization. The process performances were evaluated in terms of surface roughness which is correlated with characterization techniques such as Scanning Electron Microscopy (SEM) and Electron Backscatter Diffraction (EBSD). It was observed that electropolished and stress-relieved stent exhibits lower average surface roughness R_a ($0.484 \mu\text{m}$), root mean square of the profile R_q ($0.560 \mu\text{m}$), total height of the roughness profile R_t ($2.789 \mu\text{m}$) and ten-point mean roughness of R_z ($1.98 \mu\text{m}$), as compared to remaining samples. The average grain size is observed to be $40 \mu\text{m}$ for the electropolished stress-relieved stent. The obtained results were corroborated by the surface topography, local misorientation angle, grain size, and grain orientation. The overall study exhibits that electropolished and stress-relieved stent surface was found to be suitable.

Keywords: CVD, Stent, Selective laser melting, SS316L, Surface roughness, Metallurgical aspects

1. Introduction: -

Numerous cardiovascular diseases (CVD) have become more prevalent recently, and an increasing number of people have early-stage heart disease. Each year, countless individuals need assistance in the fight against heart disease. The most often implemented cardiovascular therapies comprise coronary artery bypass graft (CABG), heart valve replacement or repair, pacemaker insertion, heart transplantation, maze surgery, and coronary angioplasty aimed at treating cardiovascular disease. Coronary artery bypass graft (CABG) and coronary angioplasty which are the most commonly used methods for treating illnesses related to blood flow to the heart [1,2]. One of history's most important medical advancements was the discovery of coronary angioplasty. Through a procedure called coronary angioplasty, blood can once more flow to the heart by relaxing the constrictions in the coronary arteries. Andreas Grunting carried out the initial angioplasty in 1977 [3]. In this process, a catheter is inserted through a peripheral artery to deliver a balloon to the site of blood vessels narrowing. Following that, the balloon is forced to expand under pressure, which enlarges the vessel, increases lumen size, and enhances blood flow. One of the vital elements used in

coronary angioplasty is the stent. A stent is a small metal mesh tube that ensures the opened arteries will not narrow or close again [4-6].

Typically, stents are made of Stainless Steel 316 L (SS316 L), Tantalum (Ta), Nitinol (Ni-Ti), Platinum (Pr), Titanium (Ti), Cobalt-Chromium (Co-Cr), Magnesium Alloy (WE43), and Pure Iron. Stents are also made from biodegradable metals based on magnesium, iron, and zinc. SS316L is an austenitic chromium-nickel stainless containing a deliberate amount of molybdenum which generally increases and improves pitting resistance and possesses low radiopacity and a strong propensity for crevice corrosion, also its fatigue property provides adequate strength under cyclic load in a biological environment. As a result, SS316L is extensively used in biomedical implant applications, including cardiovascular stents, artificial heart valves, bone fixation, orthopedic implants, screws, pins, sutures, and steel threads used in the fixation of fractures [7-10].

As the demand for stents is increasing every year, currently various conventional and non-conventional manufacturing techniques are used in manufacturing the stent. Knitting, welding, braiding, and photochemical etching, micro-electro-discharge machining, electroforming are examples of stent manufacturing techniques. A higher percentage of stents are manufactured using laser cutting of the tubes [10-11]. Despite being used for the majority of stent manufacturing, still it is lacking in manufacturing customized and complex-shaped stents as stents made traditionally may fit most people or be one size fits all; nevertheless, certain medical conditions need specialized care. The powder bed fusion 3D printing technology stands out as an intriguing choice for this purpose, as it can be utilized to make stents straight from powder. The development of this technology has been the subject of significant research from academia and industry. 3D printing is an additive fabrication technique to produce 3D components. It has the potential to print tools and parts in the interim, zero waste, lower cost, and innate micro-manufacturing capacity, which compel it to be used for biomedical applications [12-14].

The surface integrity is vital for bioimplants manufactured by any conventional or non-conventional method. Surface integrity is defined as the inherent or enhanced surface conditions produced by a machining or other surface-generating operation. It is quantified by the mechanical, metallurgical, chemical, and topological state of the surface. Surface integrity and functional performance of manufactured components have been a significant proponent for developing new manufacturing processes [15]. Also, Grain structure plays a significant role in determining the mechanical properties of materials, particularly in metals and alloys. The grain structure significantly influences the mechanical properties of materials, including strength, ductility, toughness, hardness, fatigue resistance, and creep resistance. Finer grains generally promote higher strength, ductility, toughness, fatigue resistance, and creep resistance, while coarser grains may lead to lower values for these properties [16-18]. So it is important to analyze the surface produced by 3D printing concerning its application in bioimplants. Also, there is a lack of studies reported on surfaces originating in bioimplants due to the 3D printing process. Additionally, scarce research has been reported on the metallurgical elements of 3D-printed bioimplants.

This study examines the metallurgical properties and surface roughness characteristics of an SLM-fabricated SS316L stent. Specifically, the surface roughness was measured, and then scanning

electron microscopy (SEM) and electron backscatter diffraction (EBSD) were used to evaluate the grain size, orientation, and local intergranular misorientation. The surface roughness characteristics of four different post-processed surfaces were evaluated, and the good surface quality of the stent was taken into further consideration for the metallurgical aspect to overcome the challenges connected with employing 3D printing to make bioimplants.

2. Materials and Method

This section includes stent design, material, manufacturing process, experimental set-up, post-processed methods, their parameters and levels, and surface measurements and characterization techniques.

2.1 Stent Design and Material

SS316L powder was used in experimentation because of its simplicity in production, biocompatibility, appropriate mechanical strength, and corrosion resistance qualities. A stent with the following dimensions: length 40 mm, exterior diameter 4 mm, inside diameter 3.5 mm, the axial gap between neighboring stents 3.69 mm, and strut thickness 0.5 mm, was the subject of experiments. The stent illustrated in Fig.1 was created using the CREO CAD tool and served as an input for the SLM process used in 3D printing. To ensure that the part receives support while being printed, the stent's design is closed-structured.

Figure 1. CAD model of stent prepared in CREO

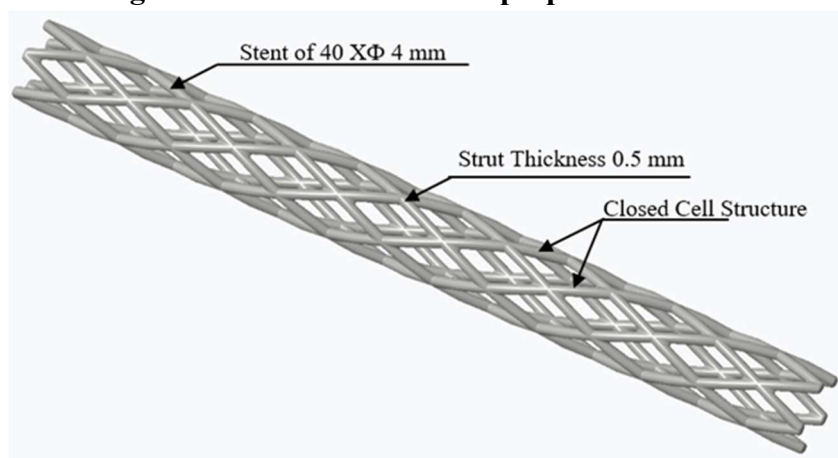


Table 1 lists the molecular composition of the SS316L powder used to create the stent. The powder used in this experimentation is prepared through a gas atomizing process (make: OEM). The powder used has a particle size range of 10 to 45 μm and a spherical particle shape. The powder had a bulk density of 7.95 g/cm^3 and a thermal conductivity of 15 W/mK .

Table 1. Material composition of SS316L powder

Elements	Fe	N	C	S	P	Si	Mn	Mo	Ni	Cr
Wt.%	bal.	11.39	0.015	0.016	0.011	0.74	1.22	2.37	11.39	17.37

2.2 SLM Setup

The industrial SLM system (make: SLM solutions SLM 280) was employed in the experimental 3D printing of the stent, as illustrated in Fig.2. Optimized input process parameters were taken into account in this work. Pre-pilot trials, preliminary experimentation, and a literature review are used to finalize the parameters. A constant layer thickness of 60 μm and height to aspect ratio of 1 mm were used in the printing of the stents. The device was configured to generate the stent at a maximum throughput of 113 cm^3/h . The process used an average of 13 l/min of inert gas, with a beam focus of 80 μm and a scan speed of 10 m/s. Further sandblasting technique was used for cleaning the powder particles from the stent. These parameters were concerning supports as the part has a low thickness. Figure 3 shows SS316L stent manufactured on SLM 280 setup.

Figure 2. SLM 280 Setup



Figure 3. 3D Printed SS 316L powder stent with SLM process



2.3 Post-Processing Conditions

In this study, four samples of the stent, S1: stress-relieved, S2: electropolished, S3: stress-relieved and electropolished, and S4: without stress-relieved and without electropolished. For Sample S1 heat treatment was carried out to relieve the stresses developed during the process, ramping up 150° per hour, holding at a temperature of 400° for two hours, and then cooling in the furnace. For Sample S2 electropolishing was carried out on the stent, the electrolyte temperature was 75° C. In the electrolyte, the perforated stainless steel cylinder served as a cathode. For electropolishing the value for current (I) = 0.6 to 0.75 A, temperature (T) = 75° C \pm 2° C, and polishing time (t) = 30 to 75 sec. The electrolyte commonly used for electropolishing SS316L stents is typically a mixture of sulfuric acid and phosphoric acid. Sample S4 was utilized in the investigation without any post-

processing procedures, while sample S3 underwent both heat treatment and electropolishing procedures.

3. Results and Discussion

In this section, the obtained results of surface roughness, surface topography, and surface metallurgical aspects in terms of grain size, grain orientation, and local misorientation are discussed.

3.1 Surface Roughness

Surface roughness influences the interaction between stents and arteries, it is an essential feature of bioimplants[19]. In this study, four samples with an 80 μm sample profile length and a 10x to 80x lens set had their average surface roughness measured using a Bruker Alicona μCMM . Figure 4(a), illustrates stress-relieved stent, which have average surface roughness of R_a (0.546 μm), root mean square of the profile of R_q (0.692 μm), total height of the roughness profile of R_t (3.618 μm) and ten-point mean roughness of R_z (2.254 μm). From Fig. 4(b), electropolished stent had an average surface roughness of R_a (0.491 μm), root mean square of the profile of R_q (0.663 μm), total height of the roughness profile of R_t (3.115 μm) and ten-point mean roughness of R_z (2.32 μm). From Fig. 4(c), stress-relieved and electropolished stent had an average surface roughness of R_a (0.484 μm), root mean square of the profile of R_q (0.560 μm), the total height of the roughness profile of R_t (2.789 μm) and ten-point mean roughness of R_z (1.98 μm) and from Fig. 4(d), without stress-relieved and without electropolished stent had an average surface roughness of R_a (2.654 μm), root mean square of the profile of R_q (3.666 μm), total height of the roughness profile of R_t (16.915 μm) and ten-point mean roughness of R_z (7.842 μm). The stress-relieved and electropolished stent exhibited lower surface roughness as compared to other samples.

Figure 4. Surface parameters: (a) Stress-relieved, (b) Electropolished, (c) Stress-relieved and electropolished, and (d) Without stress-relieved and without electropolished

Figure 4(a). Stress-relieved

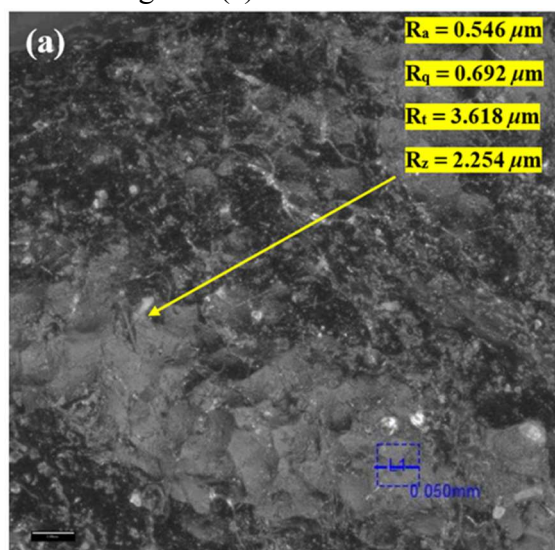


Figure 4(b). Electropolished

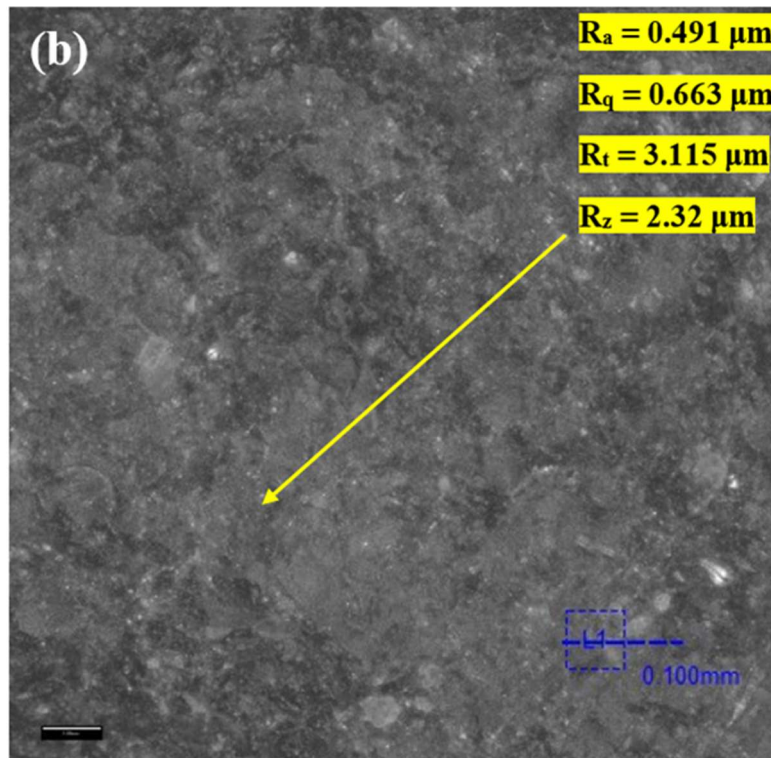


Figure 4(c). Stress-relieved and electropolished

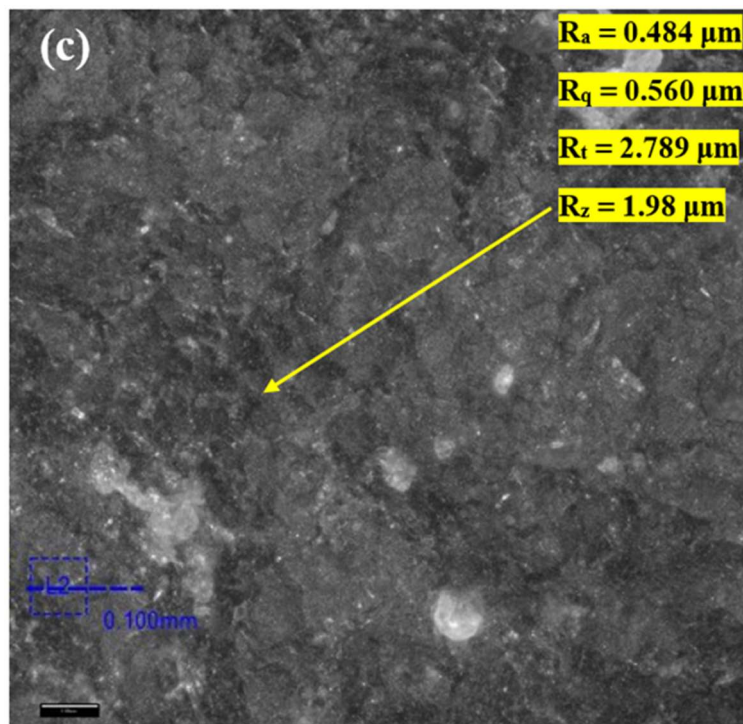
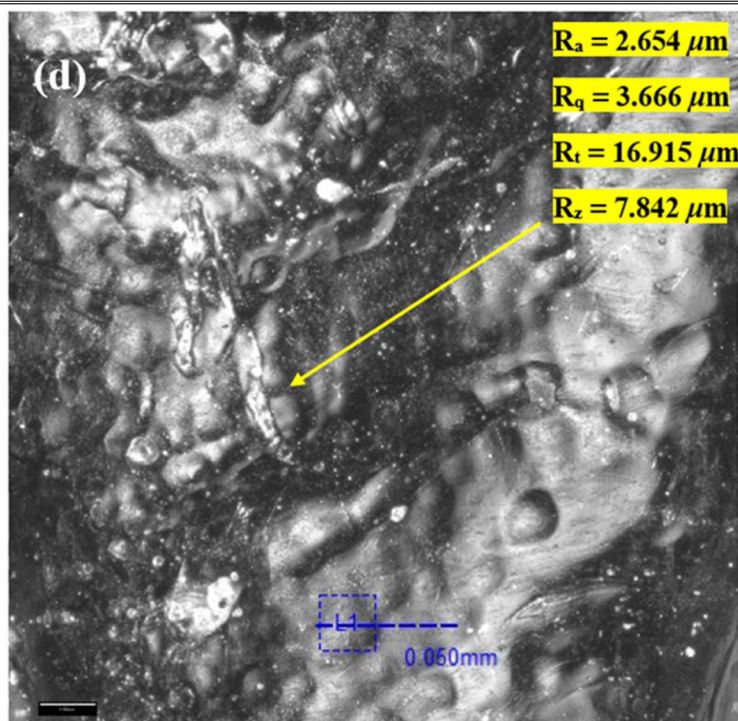


Figure 4(d). Without stress-relieved and without electropolished



3.2 Surface Characterization

It is necessary to explore the surface morphology of the SS316L stent surfaces manufactured using the SLM technique, because several instances have been noted that were brought about by post-processing operations, viz., warpage, porosity, unmelted powder, micro-cracks, and particle deposition on the stent surface produced by the SLM process. SS316L powder stent surface morphology was investigated using SEM (make: ZEISS GeminiSEM 300). SEM was conducted along the length to examine the surface morphology at 1000x magnification. Figure 5(a) shows unmelted powder particles and microcracks over the stress-relieved stent surface. Most often a 3D printed part undergoes stress-relieving, internal stresses that were present in the part are reduced or eliminated through controlled heating and cooling process. However, during this process, residual stresses are still present, particularly at the surface of the material. These stresses strive to exit the surface, resulting in the formation of microcracks [20]. The electropolished stent surface shows porous structure, shown in Fig. 5(b). Besides, Fig. 5(d) without stress-relieved and without electropolished stent exhibit deposition of powder particles on the surface. In contrast, smooth surface of the stress-relieved and electropolished stent is observed illustrated in Fig. 5(c). Because, the controlled heating and cooling eliminates process and material defects such as layer inconsistency, incomplete melting, inadequate powder bed formation, layer gaps, internal stresses, etc. These removal of defects gives even and good quality printing. Furthermore, optimized electropolishing removes unmelted particles, strays, metal deposition from the surface. Therefore, the combined effect of stress-relieving and electropolishing exhibits a better surface-quality.

Figure 5. SEM images: (a) Stress-relieved, (b) Electropolished, (c) Stress-relieved and electropolished, and (d) Without stress-relieved and without electropolished.

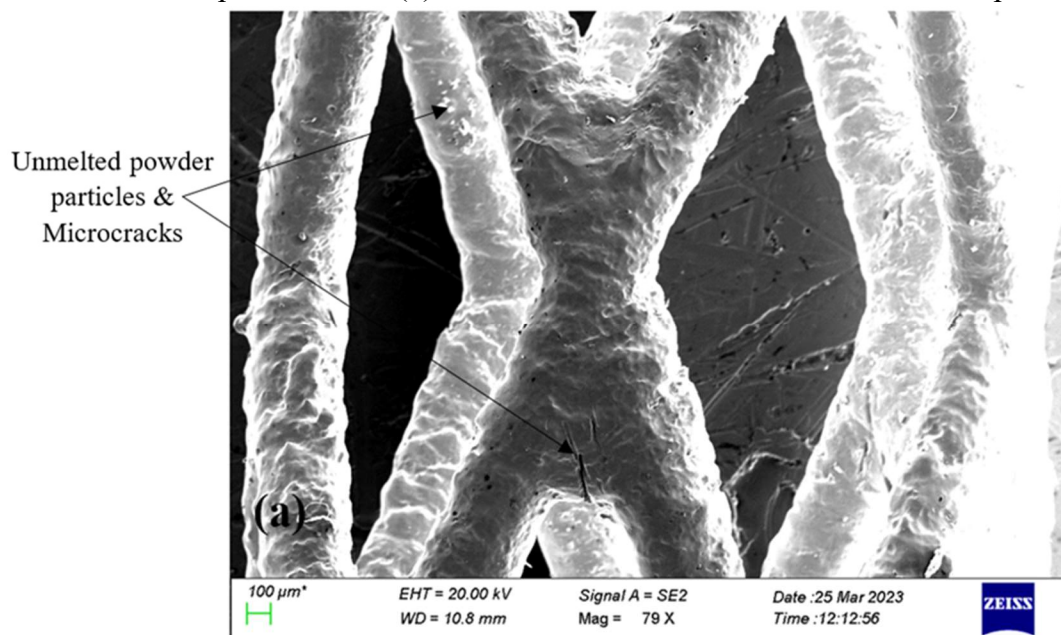


Figure 5(a). Stress-relieved

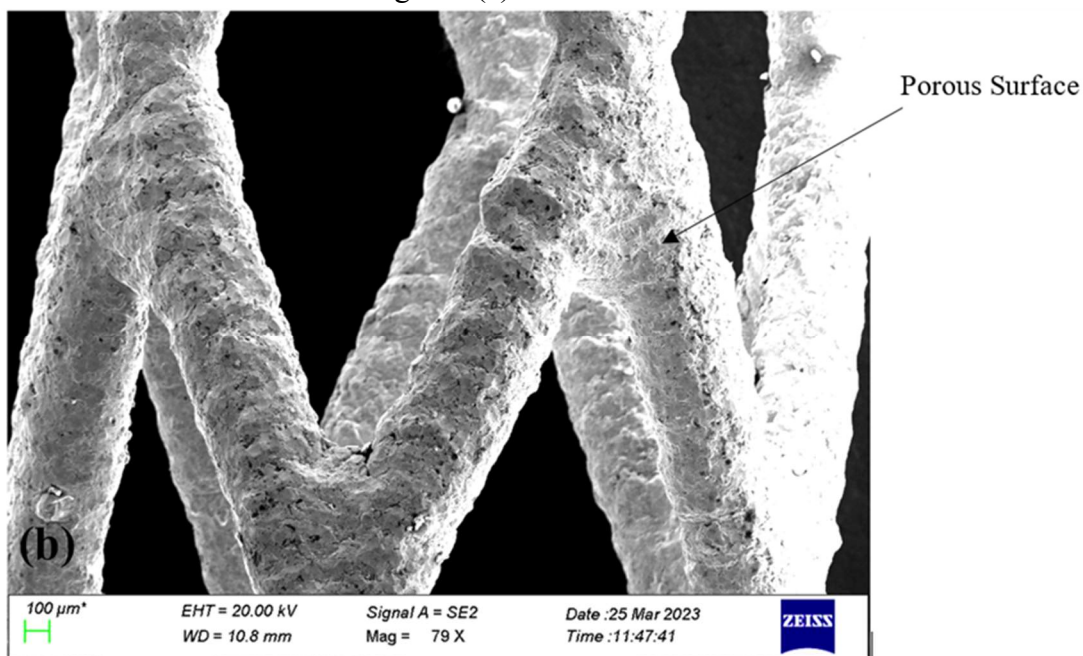


Figure 5(b). Electropolished

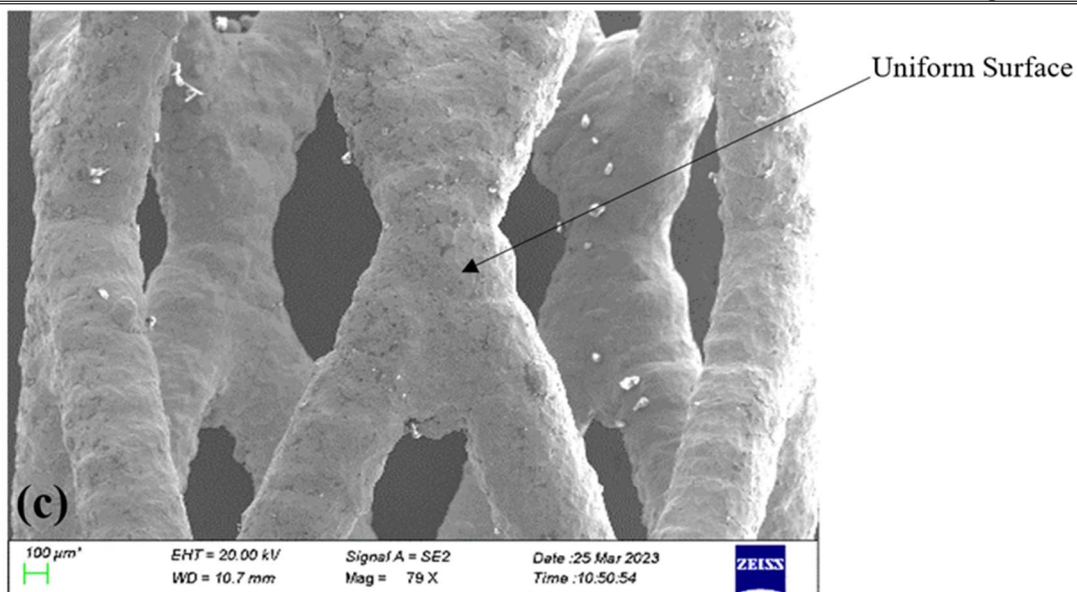


Figure 5(c). Stress-relieved and electropolished

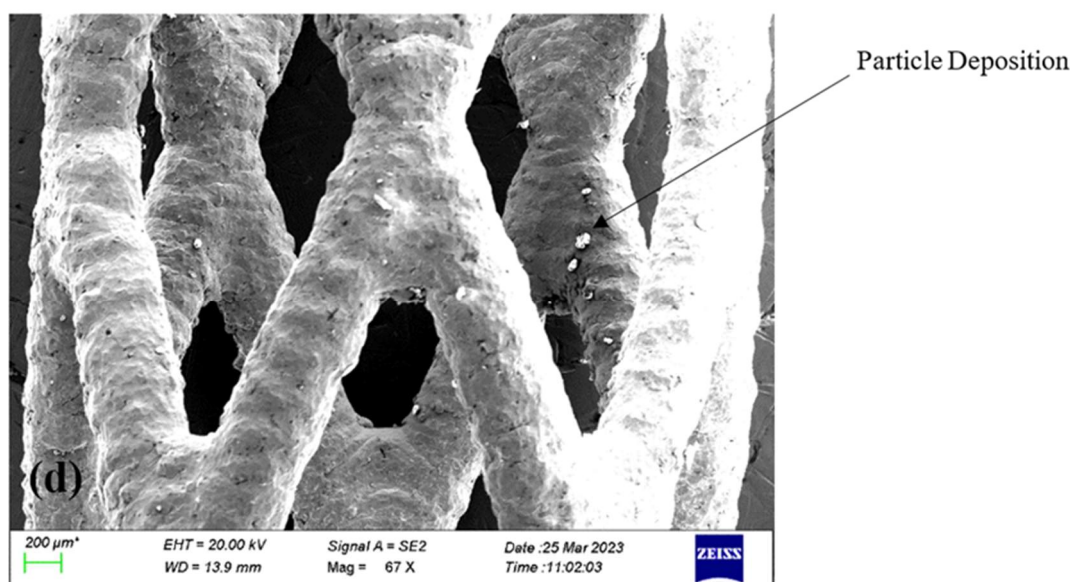


Figure 5(d). Without stress-relieved and without electropolished

3.3 Grain Size, Grain Orientation, and Misorientation Angle

The results observed from the surface roughness and surface characterization show that the stress-relieved and electropolished stent has improved surface quality as compared remaining samples. Therefore, it has been considered for further metallurgical analysis in the perspective of biomedical applications. Hence, the surface integrity of stress-relieved and electropolished stents is explored in terms of grain size, grain orientation, and misorientation angle [21]. For the preparation of the sample, the sample was grinded to remove surface imperfections and achieve a flat, polished surface. After grinding, the sample was polished using a series of finer abrasives to further refine

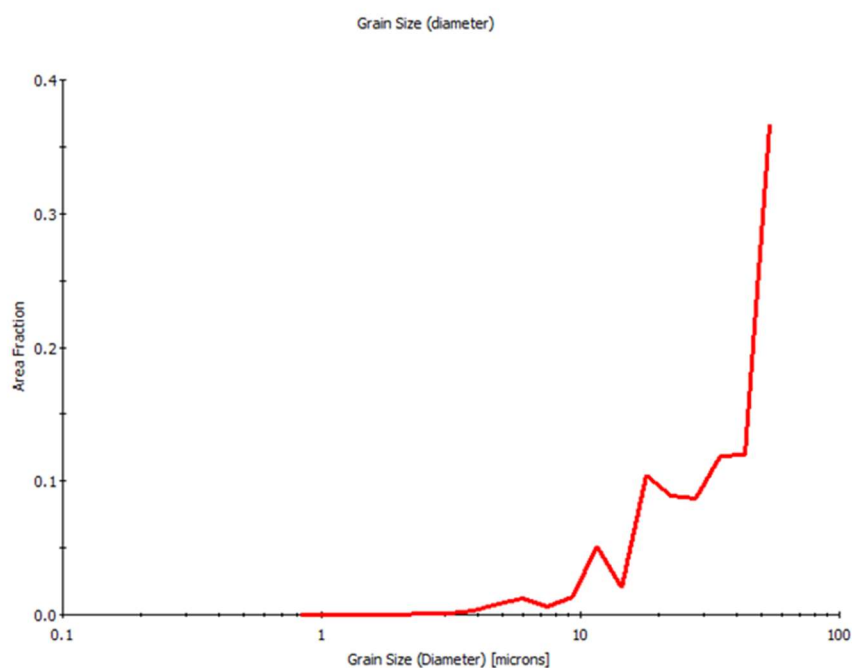
the surface and remove any remaining scratches or defects. The final polish should produce a smooth, mirror-like surface suitable for EBSD analysis and finally, the sample was thoroughly cleaned to remove any debris, contaminants, or polishing residues that may interfere with the EBSD measurements.

Metallurgical properties, including composition, phase structure, and processing conditions, profoundly influence material behavior and performance. For instance, alloying elements can alter mechanical properties and corrosion resistance, while heat treatment can modify microstructure and grain size. In cell growth, metallurgical properties can affect surface chemistry, which in turn influences cell adhesion, proliferation, and differentiation. Certain metals or alloys may exhibit biocompatibility or bioactivity, promoting favorable interactions with cells [22].

Grain size refers to the size of individual crystals (grains) in a polycrystalline material. Smaller grain sizes typically result in higher strength and hardness due to grain boundary-strengthening mechanisms. In terms of cell growth, smaller grain sizes can inhibit the movement of dislocations, which are necessary for plastic deformation and thus can hinder cell formation. However, if there are preferred sites for nucleation at grain boundaries, smaller grains may enhance cell growth. The average grain size obtained of 3D printed stent is 40 μm as shown in Fig. 6(a). The suitability of a 40 μm grain for supporting cell growth depends on several factors, including the type of cells being cultured, the intended application, and the specific characteristics of the grains themselves. In general, cell growth and adherence can be influenced by the surface characteristics of the substrate, including its texture, chemistry, and porosity. While some cells may thrive on a substrate with a grain size of 40 μm , others may require a different surface texture or size for optimal growth.

Figure 6. (a) Grain size, (b) Grain Orientation, and (c) Misorientation angle of stress-relieved electropolished stent

Figure 6(a). Grain Size



The orientation of grains refers to the crystallographic orientation of adjacent grains. Certain crystal orientations can promote the formation of cells due to their effect on dislocation movement and grain boundary energy. Favorable orientations can lead to easier slip, facilitating the formation and propagation of cells. Practically all grains are oriented in the (001) plane which exhibits the lowest hardness and elastic modulus compared to plane (111) and (101). From Fig. 6(b) 19.91% and 15.53% of the grains have an orientation towards the (111) and (101) planes, respectively, and 64.56% of the grains have a heading towards the (001). Certain grain orientations, such as those that mimic the natural extracellular matrix (ECM) of tissues, can support cell adhesion, proliferation, and differentiation. For example, materials with anisotropic grain orientation, where the grains are aligned in a specific direction, can promote cell elongation and alignment along the same direction. This alignment can be beneficial for tissues like muscles or nerves, where directional cues are important for proper function. In general, materials with microstructures that resemble the native tissue ECM, including appropriate grain orientation, can provide cues for cells to attach, proliferate, and differentiate, thus supporting cell growth and tissue regeneration.

Figure 6(b). Grain orientation

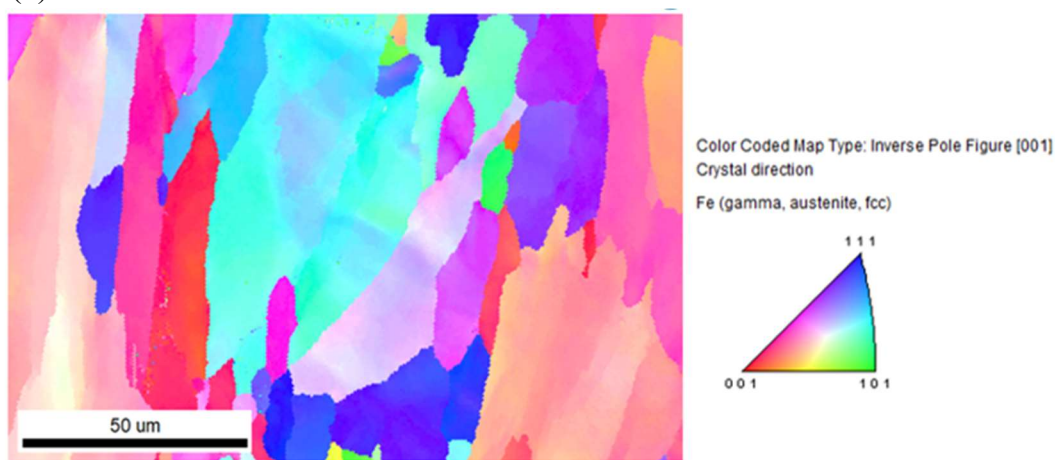
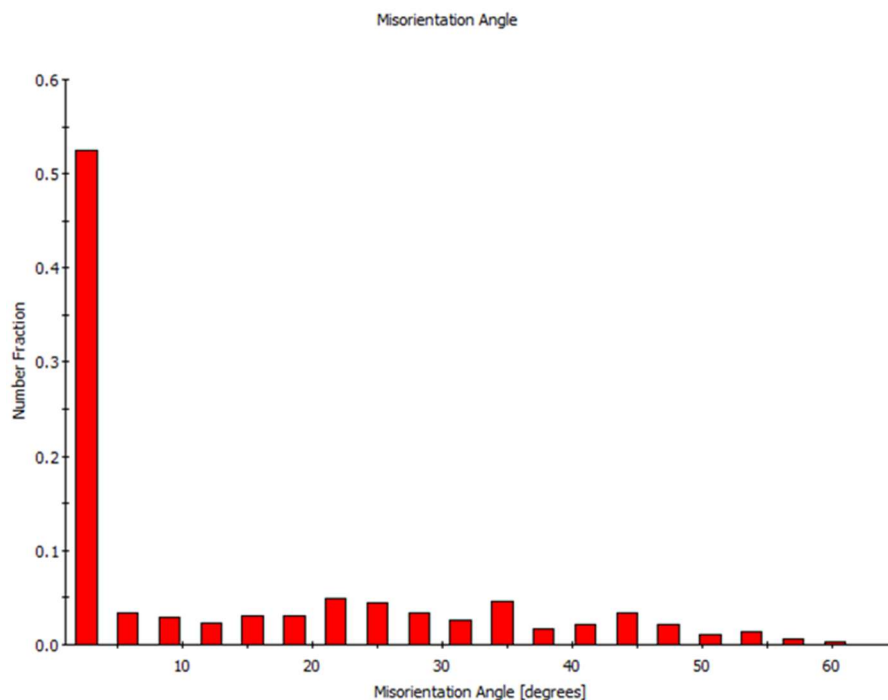


Figure 6(c). Misorientation angle



The misorientation angle refers to the angle between adjacent grains. Higher misorientation angles can lead to increased stored energy within the material, which can drive the formation of subgrains and subsequently cells. Dislocation pile-ups and interactions at high-angle grain boundaries can facilitate the formation of cells. The local grain misorientation of the electropolished and relieved stent stress is shown in Fig. 6(c). Local grain misorientation has a significant impact on the SLM process. Local grain misorientation was used to comparatively analyze the effects of the SLM procedure on surface roughness. The largest grain area fraction was discovered to be below the 5° grain misorientation angle, and roughly 64 % of the grain area fraction was found below the 15° . Overall, controlling factors in materials design (mechanical and metallurgical), facilitates the development with tailored properties specifically biomedical applications, such as stent

4. Conclusion: -

This study examined the impact of post-processing methods on surface roughness metrics and in extension, the optimized parameters are corroborated with metallurgical considerations such as grain size, grain orientation, and local misorientation in suitability with biomedical applications. From this examination following conclusions were drawn.

- The surface roughness parameters are more specific to exhibit surface quality. The surface parameters such as R_a 0.484 μm , R_q 0.560 μm , R_t 2.789 μm , and R_z 1.98 μm for stress-relieved and electropolished stent is found to be better. Whereas the surface roughness parameters as mentioned above are observed to be higher in the order of without stress relieved and without electropolished, electropolished and stress relieved, stent respectively.

- The evaluation of SEM images of surface topography of 3D printed stent surface corroborates the obtained surface parameters. The surface defects such as warpage, unmelted powder, metal deposition, and microcracks are observed in SEM images of without stress relieved and without electropolished, electropolished, and stress relieved, respectively.
- The SLM process has a significant impact on grain orientation and it exhibits the inverse relation with grain size. The average grain size is found to be 40 μm for the electropolished stress-relieved stent.
- Grain orientation which is important to study hardness and elastic modulus of the material, showed that grains were close to 001.

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